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Anisotropic and temperature-dependent growth mechanism of *S*-phase precipitates in Al−Cu−Mg alloy in relation with GPB zones

Mei-jie YIN, Jiang-hua CHEN, Shuang-bao WANG, Zi-ran LIU, Li-mei CHA, Shi-yun DUAN, Cui-lan WU

College of Materials Science and Engineering, Hunan University, Changsha 410082, China

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Abstract: By employing atomic-resolution imaging and first principles energy calculations, the growth behavior of *S*-phase precipitates in a high strength Al−Cu−Mg alloy was investigated. It is demonstrated that the nucleation and growth of the *S*-phase precipitate are rather anisotropic and temperature-dependent companying with low dimensional phase transformation. There are actually two types of Guinier−Preston (GP) zones that determine the formation mechanism of *S*-phase at high aging temperatures higher than 180 °C. One is the precursors of the *S*-phase itself, the other is the structural units or the precursors of the well-known Guinier–Preston–Bagaryatsky (GPB) zones. At high temperatures the later GPB zone units may form around *S*-phase precipitate and cease its growth in the width direction, leading to the formation of rod-like *S*-phase crystals; whereas at low temperatures the *S*-phase precipitates develop without the interference with GPB zones, resulting in *S*-phase precipitates with lath-like morphology. **Key words:** aluminum alloy; precipitation; age hardening; anisotropy; crystal growth

1 Introduction

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For nearly 100 years the AA2024 Al−Cu−Mg alloys have been important materials for the aerospace industry due to their excellent strength and plasticity [1,2]. As one of the widely used age-hardenable aluminum alloys, both their precipitate characteristics, such as the morphology, the crystallographic orientation and the structure type of the precipitates, and their precipitation behaviors during ageing treatments have been important issues for understanding the relations between the properties and the processes of the alloys [3−30].

In high-strength Al−Cu−Mg alloys with relatively high Mg/Cu ratios, like the AA2024 (Al−4.57Cu− 1.34Mg, mass fraction, %) alloy investigated in the present study, three types of fine precipitates may form. The first type of precipitates that always form upon ageing is the solute clusters. They are structurally less ordered and therefore are less effective in hardening the alloys. They can be visualized in atom-probe ion-field microscopy [5−8] but normally cannot be seen in scanning transmission electron microscopy (STEM) and in high-resolution transmission electron microscopy (HRTEM). The second type of precipitates that may form in the alloys is the 1D crystals, known as Guinier−Preston−Bagaryatsky (GPB) zones [8−11], as illustrated in Figs. $1(a)$, (b) and (d). The GPB zones are effective hardening particles and can form rapidly if ageing temperature is higher than 190 °C. Their formation can be depressed if the alloys are aged at 180 °C or below. Significant progresses have recently been achieved in characterizing their structures with STEM [3,4,9] after pioneer made efforts with different tools [5,6,12−16]. One GPB zone is usually assembled by more than one GPB units (Fig. 1(d)). The third type of precipitates in the Al−Cu−Mg alloys is the most effective strengthening particles known as *S*-phase precipitates (Figs. 1(a)−(c)). They are 3D-nanocrystals of an equilibrium phase with a composition of Al_2CuMg . Their typical morphology is either lath-like or rod-like, depending on aging temperature and aging duration. The *S*-phase precipitates have a principle orientation relationship (OR) with the matrix [27], but can be tolerant of a few degrees of deviation from their principle OR [17−26]. The *S*-phase is of a centered-orthorhombic crystal structure, as originally proposed by PERLITZ and WESTGREN [27].

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Corresponding author: Jiang-hua CHEN; Tel: +86-731-88664009; E-mail: jhchen123@hnu.edu.cn DOI: 10.1016/S1003-6326(16)64082-7

It has generally been believed that the GPB zones, or somewhat different phases named by "*S*" [11,13,21], are the precursors of the *S*-phase, though significant controversies have long existed about the formation of *S*-phase precipitates [5−8,11−13,15−17,20,21]. According to our recent study [3], the *S*-phase precipitates always have, without exception, an even number of Cu−Mg atomic-layers that parallel to the $(210)_{\text{Al}}$ plane (perpendicular to its thickness). In this way, an *S*-phase precipitate can be specified by its thickness or the number of Cu−Mg atomic-layers in the precipitate, e.g., an *S*2*n* precipitate means that it contains 2*n* Cu−Mg atomic-layers in thickness. An *S*2 precipitate contains two Cu−Mg atomic-layers in thickness and is the thinnest *S*-phase precipitate. So, the nucleation and growth of an *S*-phase precipitate can be understood in details. It has been shown [3] that driving by energy decrements, the main precipitation sequence towards *S*-phase formation is as follows: SSSS→GP*S*2-I(Al3MgCu)→ GP*S*2-II $(Al_2MgCu) \rightarrow S_2 (Al_2MgCu) \cdots \rightarrow S_{2n}$, where SSSS stands for super-saturated solid solution, GPS₂-I and GPS₂-II are the precursors (GP zones) of an S_2 precipitate (Fig. 1(e)). This implies that the formation of *S*-phase is independent of the GPB zones, at least for low temperature aging [3].

However, at a higher temperature (above 190 °C) the *S*-phase precipitates and the GPB zones may nucleate and grow simultaneously. In this case, the two types of precipitates must compete for their developments. Interestingly, it has been observed that the structure of one type of GPB zones has a close relation with the *S*-phase structure [9,10]. Hence, to date, the following questions still remain unclear: 1) how do the GPB zones interfere the development of the *S*-phase precipitates? 2) At above 190 °C, will an *S*-phase crystal grow in the same manner as it develops at a lower temperature? 3) Can an *S*-phase precipitate be formed based on a pre-existed GPB zone?

In the present work, using atomic-resolution imaging and first principles energy calculations, we investigated the *S*-phase precipitates for their growth mechanism and temperature-dependency, as well as for the influence of the co-existed GPB zones on their morphology. It is shown that advanced high-angleannular-dark-field (HAADF) imaging in STEM, in combination with recent progresses in the structure determination of early-stage *S*-phase precipitates zones [3,4] and GPB zones [9,10], has made it possible to well understand the relations between the two important types of hardening precipitates in the Al−Cu−Mg alloys.

2 Experimental

2.1 Alloy samples and thermal aging

The materials used in the present work were supplied in the form of homogenized rolled sheets and had a composition of Al−4.57Cu−1.34Mg−0.81Mn (mass fraction, %). Prior to the hardening age, the alloy was solution heat-treated at 495 °C for 1 h and then water quenched to room temperature $(20 \degree \degree C)$. Subsequent thermal aging was carried out in an oil bath at 20, 130, 150, 180, 190, 200, 220 and 250 °C, respectively. Specimens for the STEM and HRTEM

Fig. 1 Illustrative overviews of *S*-phase and GPB zones formed in AA2024 alloy upon thermal aging: (a) *S* precipitates and GPB zones (shown in inset) formed after aging at 220 °C for 20 min, viewed along [100]_{Al}; (b) 3D schematic of bunches of *S*-phase particles and GPB zones in Al-matrix, typical morphology of lath-like *S*-phase particle with thickness *t*, width *W*, and length *L*; (c, d) Typical HRTEM images of *S*-phase (c) and GPB zone (d); (e) Fine precipitation scenario of *S*-phase precipitate that evolves structurally from its precursors GP*S*₂-I to GP*S*₂-II, then to *S*₂-structure and then grows thicker into *S*₄ precipitate [3]

observations were prepared first by mechanical polishing and then by electro-polishing until perforation.

2.2 Atomic-resolution imaging in electron microscopy

2.2.1 High-resolution transmission electron microscopy (HRTEM) image

An FEI Tecnai F20 HRTEM and a JEOL 3010 HRTEM instruments, operating at 200 and 300 kV respectively, were employed in the present study. Two atomic-resolution imaging techniques are available with the FEI Tecnai F20 HRTEM microscope: one is to perform through-focus exit-wave function reconstruction (TF-EWR) over focus-variation series of about 20 images per series that are automatically recorded in the HRTEM imaging mode [31−34]; the other is to perform high-angle-annular-dark-field (HAADF) imaging in the STEM imaging mode. The highest point resolution of the microscope achievable by performing TF-EWR is 0.14 nm (information limit) [35], while its best point resolution achievable in HAADF−STEM is 0.16 nm. The key issue of performing atomic-resolution imaging was to obtain images that reflect truly the real atomic structures of the observing objects (within the resolution limitation of the microscope).

2.2.2 HAADF imaging in STEM

In the HAADF−STEM imaging mode, the obtained image shows a *Z*-contrast (where *Z* represents the atomic number of the atoms in the specimen) proportional to $Z^{1.7-2.0}$ [36–38]. Hence, the HAADF image contrast is relatively easy to interpret in terms of the structure, so long as the composition of the observing material is known, though the light atoms are more difficult to be visualized than the heavy atoms when they are largely different in *Z* and co-exist in the structure. The imaging parameters are as follows: operating at 200 kV, with a half-angle of about 12 mrad for probe convergence and with a collection inner semi-angle of 36 mrad.

2.3 First principles energy calculations

The first-principles calculations were performed using density functional theory (DFT) implemented in the Vienna ab initio simulation package (VASP) with efficient ultrasoft pseudo potentials [39−43]. The generalized gradient approximation (GGA) with the exchange-correlation functional of PERDEW [44,45] was employed. Convergence tests indicated that 260 eV was a sufficient cutoff for the ultrasoft pseudo potential to achieve high precision in the Al−Cu−Mg system. For all structures, *k*-points sampling using Monkhorst−Pack method [46] was increased to reach the precision of 0.1 kJ/mol. The thermal contributions and zero-vibration energy differences or contributions were ignored because of their little effect on this alloy system [4]. Sufficiently large super cells were used in all calculations in order to

include the interface energy and the strain energy for the particles [4]. The formation enthalpies were defined and calculated in kJ/mol per solute atom [47].

The formation enthalpy (with thermal contributions and zero-vibration energy difference or contribution being ignored) for an equilibrium phase $Al_xCu_yMg_z$ can be defined as [48]

$$
\Delta H(\text{Al}_x\text{Cu}_y\text{Mg}_z) =
$$

$$
E(\text{Al}_x\text{Cu}_y\text{Mg}_z) - x_{\text{Al}}E(\text{Al}) - y_{\text{Cu}}E(\text{Cu}) - z_{\text{Mg}}E(\text{Mg}) \qquad (1)
$$

where $E(A\text{I}_{x}Cu_{y}Mg_{z})$ is the total energy of $A\text{I}_{x}Cu_{y}Mg_{z}$ phase per atom, obtained by first-principles calculations. *E*(Al), *E*(Cu) and *E*(Mg) are energies for pure elements Al, Cu and Mg, respectively. $x_{\text{Al}}=x/(x+y+z)$, $y_{\text{Cu}}=y/(x+y+z)$ and $z_{\text{Mg}} = z/(x+y+z)$ are the fractional compositions of Al, Cu and Mg, respectively.

To include thermal contributions to the stability of *S*-phase at a finite temperature, both lattice thermal vibration and thermal electrons should be considered. The Helmholtz free energy (*F*) with an average atomic volume (V) at a temperature (T) can be obtained by [49,50]

$$
F(V,T)=E_c(V)+F_{vib}(V,T)+F_e(V,T)
$$
\n⁽²⁾

where E_c is the energy (without zero-point vibration energy) obtained from first-principles calculations at 0 K; F_{vib} is the free energy for lattice vibration, which can be calculated with the quasi-harmonic approximation through employing the plane-wave self-consistent field (PWSCF) method [51] based on the ab initio linearresponse theory [52−55]. Using the linear-response theory approach for one unit cell, the phonon frequencies can be found without much computation. F_e is the free energy of thermal electrons, which can be obtained via 1D numeric integrations over the electronic density of states (calculated using VASP) following the Fermi distribution [49,50].

We calculated all the zero-vibration energies (E_{zero}) for the related structures at 0 K using VASP, and obtained the values 3.4, 2.8, 3.1 and 4.8 kJ/(mol·atom) respectively for the *S*-phase (Al₂MgCu), FCC-Al, HCP-Mg and FCC-Cu crystals. Their contribution to the formation enthalpy, $ΔE_{zero}=4ΔE_{zero}(A₁₂CuMg)−$ 2Δ*E*zero(Al)−Δ*E*zero(Mg)−Δ*E*zero(Cu)≈0.1 kJ/(mol·atom), is rather small, as compared with other contributions, and therefore is negligible in these calculations.

3 Results and discussion

3.1 Hardening responses of alloy at different aging temperatures

Figure 2 shows the hardness of the AA2024 alloy samples aged at various temperatures vs aging time. We roughly divided the samples into two groups: the group

of low temperature (LT) samples aged at temperatures ranging from 20 to 180 °C, and the group of high temperature (HT) samples aged at temperatures ranging from 190 to 250 °C.

Fig. 2 Age-hardening curves of alloys aged at different temperatures against aging time: (a) LT samples; (b) HT samples

It is seen that the age-hardening responses of the LT samples (Fig. 2(a)) and the HT samples (Fig. 2(b)) are characteristically different. Figure 2(a) shows that upon thermal aging the LT samples (apart from the RT-sample) first demonstrate a rapid increase in hardness within 10 min, and then show a rather flat hardness plateau before reaching their peak hardness values. For the HT samples, it can be seen that upon thermal aging at above 190 °C, the HT samples generally demonstrate a faster increment in hardness. The hardness plateau observed among the LT samples becomes less and less obvious, and eventually vanishes for the sample aged at 250 °C. From previous studies, it is known that the highest hardness peaks are mainly due to the formation of *S*-phase precipitates, whereas the hardness plateaus are mainly due to the formation of the precursors of *S*-phase precipitates. Hence, Fig. 2 indicates that the nucleation and growth of the *S*-phase precipitates accelerate as the ageing temperature increases.

On the other side, in terms of hardness the sample aged at 180 °C demonstrates the highest hardness peak, indicating that near this aging temperature the *S*-phase precipitates can be formed mostly efficiently from the solute clusters and its precursors pre-exist in the matrix. Although the kinetics of the *S*-phase formation is enhanced in the samples being aged at temperatures above 180 °C, the hardness peaks achievable become lower and lower with the increase of temperature, implying that parallel to the formation of *S*-phase precipitates, other stable precipitates, which are less effective in strengthening the alloy with respect to the *S*-phase precipitates, are formed to have shared the super-saturated solute atoms in the matrix. These property variations will be reflected by the differences in precipitate microstructures, such as precipitate types and morphology of these samples.

3.2 Features of precipitate microstructures at different aging temperatures

Figure 3 shows the HRTEM images of typical precipitates formed in the LT and HT samples. It is shown that at 180 °C the GPB zones develop much more slowly than the *S*-phase precipitates and they appear at very late stages after the *S*-phase precipitates have fully developed, whereas at 220 °C very tiny GPB zones can be observed within a few minutes of aging. Figure 3(e) also demonstrates that since the GPB zones are 1D needle-like precipitates and are very small in cross-section at the early-stage of ageing, HRTEM imaging is not very handy to characterize their features, as compared with HAADF−STEM imaging.

Employing HAADF−STEM imaging, Figs. 4(a) and (b) demonstrate the featured difference between an *S*-phase precipitate, whose morphology is typically lath-like, formed in the LT samples and that typically with a rod-like morphology formed in the HT samples. In these atomic-resolution HAADF images of *Z*-contrast, the heavy Cu atoms in the precipitates are clearly seen. The *S*-phase precipitates formed at HT are frequently surrounded by "triangle-like" Cu clusters when they are visualized in HAADF images, as shown in Fig. 4(b). These "triangle-like" Cu clusters are actually the fundamental structure units of the well-known GPB zones as revealed in the recent literatures [9,10] and we therefore refer them to GPB units hereafter. Figures 4(c) and (d) show two possible structures of a GPB unit and energetically the one shown in Fig. 4(d) is more stable [9,10]. The GPB unit is actually a needle-like structure component growing along $\langle 100 \rangle$ _{Al} direction in 3D mode (Fig. 4(e)). When a few GPB units develop together, they will form various GPB zones structurally different in cross-section [9,10].

Fig. 3 HRTEM images of precipitate microstructures of AA2024 Al−Cu−Mg alloys upon thermal aging: (a) Early-stage precipitates of *S*-phase formed in sample aged at 180 °C for 6 min; (b) Well-developed *S*-phase precipitates formed in sample peak-aged at 180 °C for 18 h; (c) GPB zones formed in sample aged at 180 °C for about 18 h; (d) Same as (a) but aged at 220 °C; (e) Very tiny GPB zones formed in sample aged at 220 °C for 6 min; (f) GPB zones formed in sample aged at 220 °C for 20 min

Fig. 4 Atomic-resolution HAADF−STEM images of one typical lath-like *S*-phase precipitate formed in sample peak-aged at 180 °C for about 18 h (a) and one typical rod-like *S*-phase precipitate formed in sample peak-aged at 220 °C for about 0.6 h (b), which is characteristically surrounded by featured tiny GPB units; atomic structure models (c, d) of GPB unit, and energetically model shown in (d) with Al-atom between two Cu atoms in unit shifted upwards by 0.5*a* is more favored [9,10], and 3D illustration of GPB unit (e)

For more examples of the interference of GPB zones and GPB units with the *S*-phase precipitates at elevated temperatures (190−250 °C), Fig. 5 shows other three atomic-resolution HAADF images taken from the samples aged at 220 °C for 1 h and 8 h, respectively. It is seen that in a HT sample the formation of *S*-phase precipitates is frequently accompanied by the formation of the GPB zones or the GPB units. From these images

Fig. 5 HAADF images showing interaction among GPB units and *S*-phase precipitates in HT samples aged at 220 °C for 1 h (a, b) and 8 h (c) (Arrows indicate GPB zones or GPB units formed together with *S*-phase precipitates; two S_6 +GP*S*₂-II′ precipitate complexes marked in (a) and *S*18 and *S*22 precipitates marked in (c) are to notice again fact that all *S*-phase precipitates have, without exception, even numbers of Cu−Mg layers in $(210)_{Al}$ plane, as revealed in our previous work [3])

the following conclusions can be drawn. 1) Unlike those in a LT sample, the GPB zones can develop simultaneously as the *S*-phase precipitates form in a HT sample. 2) The GPB units strongly interfere with the growth of an *S*-phase precipitate in a HT sample, such that the precipitate complexes of GPB+*S*-phase can be formed frequently. For such complexes, if the core parts of *S*-phase are large, they can be recognized as *S*-precipitates (Figs. 5(a) and (c)); however, if the core parts of *S*-phase are small and the surrounding GPB zones and GPB units occupy a large portion (Fig. 5(b)), such a complex may easily be recognized as a GPB zone, especially when viewed in the conventional HRTEM imaging mode. 3) Although quick formation of GPB units around an *S*-phase precipitate has a strong influence on the development of the *S*-precipitate, the formation of *S*-phase precipitates in a HT sample seems to still follow the same fundamental rules as they form in a LT sample [3]: *S*-phase precipitates can grow thicker only through forming its precursor, the GPS_2 -II' zone, on its side (Fig. 5(a)). Since a GPS_2-II' zone has two Cu−Mg-atomic layers, all *S*-phase precipitates developed always have, without exception, even numbers of Cu−Mg-atomic layers in the $(210)_{\text{Al}}$ plane, as shown in Fig. 5(c) by the two marked *S*-precipitates, S_{18} and S_{22} . Hence, to accurately understand how the GPB units interfere with the *S*-phase precipitates in their developments, their early-stage structures have to be examined and studied in more details by using atomic-resolution imaging in association with first principles energy calculations. It is worth noting that in HAADF-STEM images, although the GPS2 zones and the *S*2 precipitates show very similar morphologies, their apparent and intuitive differences are in the separation distances between their two Cu-layers parallel to the $(210)_{\text{Al}}$ planes [3]. The S_2 precipitates have the shortest separation distance between their two Cu-layers parallel to the $(210)_{A1}$ planes.

3.3 Anisotropic and temperature-dependent growing mechanism of *S***-phase**

Figure 6 shows the *S*-phase precipitates growing in thickness in their early stage at an elevated temperature of 220 °C. It can be seen that there are actually two variants of the GPS₂-II zones attached to the thickening *S*-precipitates during their transformation from the GPS₂-II zone structure to the S_2 structure: one is the standard GP S_2 -II structure, the other refers to GP S_2 -II' structure. Their subtle difference is in that one of the two

Fig. 6 HAADF images showing *S*-phase particles growing in their thickness direction through forming GP*S*₂-II' and GP*S*₂-II structures on their sides, observed in samples aged at 220 °C for 6 to 10 min: (a) $GPS₂$ -II structures on $S₂$ precipitates; (b) GPS_2 -II and GPS_2 -II' structures being simultaneously observed on *S*-phase precipitates

Cu−Mg-atomic layers in the GP*S*2-II′ structure has become part of or integrated into the *S*-phase structure, whereas none of the two Cu−Mg-atomic layers in the GP*S*₂-II structure has been integrated into the *S*-precipitates, as demonstrated clearly in Fig. 7.

Figure 7 illustrates the detailed thickening transformation stages from S_4 +GP S_2 -II complex precipitate to the S_6 -precipitate and the calculated formation enthalpies of each meta-stable structure. From Fig. 7, we can see the following points. 1) Energetically, a GPS₂-II zone precipitate prefers to forming on the side of an existing *S*-precipitate rather than forming independently in the nearby matrix area. 2) When attached on the side of the *S*-precipitate, the contacting Cu−Mg-atomic layer of the GPS₂-II zone can easily become a Cu−Mg-layer of the *S*-phase structure, forming the meta-stable GPS₂-II' structure. These subtle intermediate stages have not been observed previously in the LT samples. The final transformation from the S_4 +GP*S*₂-II' structure to S_6 requires the Cu-atoms in the outwards Cu−Mg-atomic layer to shift upwards collectively by 0.5*a* and therefore needs more incubation time to complete, as discussed in our previous work [3].

To know the temperature influence on the formation of *S*-phase precipitates, Fig. 8 shows the free energies of the S_2 +GP S_2 -II' complex precipitate (Fig. 8(a)) and *S*4-precipitate (Fig. 8(b)) as function of temperature (Fig. 8(c)). It can be seen that the higher the temperature is, the more stable the *S*-phase precipitates are. Nonetheless, the relative stability of an S_2 +GP*S*₂-II' complex precipitate with respect to its counterpart *S*4-precipitate is larger at a higher temperature than that at a lower temperature. This may partly explain the fact that the S_2 +GP S_2 -II' complex precipitates are more

Fig. 7 Illustration of thickening transformation stages from S_4 +GP*S*₂-II precipitate complex to S_6 -precipitate and calculated formation enthalpies of each meta-stable structure

frequently observed in the HT samples than in the LT samples, though they are not very sufficient.

To see how the *S*-phase growth at an elevated temperature is different from that at a low temperature, Fig. 9 shows more featured S_{2n} +GP*S*₂-II' complex precipitates that are very frequently observed in HT samples rather than in the LT samples. Firstly, it can be noticed that at each of the two ends of a GP*S*₂-II' zone there is always a GPB unit formed with characteristic orientation, forming actually a $(S_{2n}$ +GP*S*₂-II' + GPB-unit) complex of triple components. Secondly, the width of such a GP*S*₂-II' zone varies with the number of unit cells of the GPS₂-II' structure between the two paired GPB units at its two ends. It can be speculated that in the HT samples the growth of a GPS_2 -II' zone in its width direction will be restricted by the quick formation of the

Fig. 8 Gibbs free energies (c) of S_{2n} +GP*S*₂-II' complex precipitate (a) and S_{2n} -precipitate with *n*=2 (b) in super cell models against temperature, calculated by first-principles energy calculations

Fig. 9 Atomic-resolution HAADF images of early-stage growing *S*-phase precipitates in HT sample aged at 220 °C for 6 min (a), 10 min (b) and 1 h (c), respectively $(S_2 + GPS_{2n} - II + GPB$ -unit complexes attached on sides of growing *S*-phase precipitates are indicated by arrows) and average values of statistically measured aspect ratios of *S*-phase precipitates formed at 220 °C and 180 °C against aging time (d)

two paired GPB units at its two ends. As such, the $(GPS₂-II'+GPB-unit)$ complex attached to the side of *S*-phase precipitate can only grow in its length in order to reach a critical area for its final transformation to the *S*2-structure. This provides another reason why S_{2n} +GP*S*₂-II′ complex precipitates are more frequently observed in the HT samples than in the LT samples, since the $GPS₂-II'$ components are much longer in average before being transformed to the $S_{2n}+S_2$ -precipitate. For the same reason, it can be expected that the average aspect ratio (width-to-length ratio) of the *S*-phase precipitates formed in the HT samples will be smaller than that formed in the LT samples, i.e., the *S*-phase precipitates in the HT samples will be more rod-like, whereas those in the LT samples will be more lath-like. To confirm the above speculation about the morphology of *S*-phase precipitates, we measured statistically the average aspect ratios of *S*-phase precipitates in comparison, as shown in Fig. 9(c) for the result.

From these observations on the precipitate

microstructures and their evolution with aging time and aging temperature, it can be understood that due to the quick formation of the GPB zones and the GPB units around the major hardening precipitates of *S*-phase in the HT samples, not all the supersaturated solute atoms of alloying elements, Cu and Mg, would contribute to the formation of the most effective hardening *S*-phase precipitates and therefore the height of hardness peaks will be lowered with increasing aging temperature (Fig. 2).

To summarize the difference between the anisotropic *S*-phase growth at an elevated temperature and that at a lower temperature, Fig. 10 illustrates the evolution paths of a thickening *S*-phase precipitate in a 3D view, which are subtly different depending on the aging temperature. The major reason for the difference is that during the nucleation and growth of the *S*-phase precipitate at an elevated temperature, the simultaneously formed GPB units will quickly cease the widening of the GP*S*2-II zones that are the inevitable precursors of the

Fig. 10 Comprehensive 3D illustration of anisotropic and temperature-dependent growth mechanism of *S*-phase precipitates in AA2024 Al−Cu−Mg alloys

S-phase precipitate not only for its nucleation but also for its thickening growth. Since the limitation of the GP*S*₂-II zones in width is imposed quickly by GPB units, they tend to grow more easily in length in order to reach the critical area required for their final transformation to the *S*2-structure during the whole stages of nucleation and growth of the *S*-phase precipitate. As the result of such a growth mechanism, in the HT samples the *S*-phase precipitates are more rod-like and also their average aspect ratios are smaller, as compared with those in the LT samples.

4 Conclusions

1) Using atomic-resolution imaging by HRTEM and STEM in association with first principles energy calculations, we systematically investigated the anisotropic and temperature-dependent growth mechanism of the *S*-phase precipitates in a typical AA2024 Al−Cu−Mg alloy in relation with its age-hardening responses. The one-dimensional GPB zones were studied and correlated with the formation of *S*-phase precipitates.

2) Consistent with the age-hardening responses of the alloy, the precipitate formation is temperaturedependent. At aging temperature below 180 °C, the formation of *S*-phase precipitates precedes that of GPB zones. With increasing aging temperature, the formation of GPB zones will be accelerated rapidly. At aging temperature above 220 °C, the *S*-phase precipitates and

the GPB zones will form simultaneously in the alloy and strongly interfere with each other in structure and morphology.

3) The growth of *S*-phase precipitates in the Al-matrix is rather anisotropic due to their crystallographic features, and is also temperaturedependent due to the interference of the GPB zones at elevated aging temperatures. As such, the *S*-phase precipitates formed below 180 °C are more lath-like and those formed at elevated aging temperature are more rod-like.

4) The relation between the *S*-phase precipitates and the GPB zones in typical AA2024 Al−Cu−Mg alloys has not yet been convincingly clarified so far in literature. We demonstrated the following points about this issue: on one hand, at whatever a low or a high temperature, the *S*-phase precipitates can nucleate and grow independently without the existence of GPB zones. On the other hand, at a high temperature when two types of precipitates form simultaneously, the *S*-phase precipitates and their precursors $(GPS₂ zones)$ can quickly be surrounded by the GPB zone units, forming the $GPB-GPS₂$ complexes. As such, when the core part of such a complex is in a larger portion, it may be recognized as an *S*-phase precipitate; whereas when the core part occupies only a very small portion of the complex, it may be seen as a GPB zone containing *S*-phase structure components. The existence of such complexes does not indicate that a GPB zone can directly transform to an *S*-phase precipitate, and vice versa.

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温度作用下与 **GPB** 区相关的 **Al−Cu−Mg** 合金中 *S* 相的各向异性生长机制

尹美杰,陈江华,王双宝,刘自然,茶丽梅,段石云,伍翠兰

湖南大学 材料科学与工程学院,长沙 410082

摘 要:采用原子分辨率成像和第一性原理计算,研究 *S* 析出相颗粒在高强 Al−Cu−Mg 合金晶粒内部的生长行为。 结果表明, S 相的形核和生长具有很强的各向异性特征和受温度影响的特征,同时伴随低维相转变。事实上, 在 较高的时效温度下(高于 180 °C),存在两种特征的 GP 区, 它们决定 *S* 相晶体的生长机制。一种是 *S* 相本身的前驱 体相,另一种是 Guinier–Preston–Bagaryatsky (GPB)区的结构单元或其前驱体相。在较高温度下, GPB 区的结构单 元会在 *S* 相周围形成,并阻碍 *S* 相沿宽度方向的生长,导致 *S* 相长成柱状晶体;而在低温下,*S* 相的生长不受 GPB 区的干扰,形成板条状形貌。

关键词:铝合金; 析出相; 时效强化; 各向硬性; 晶体生长

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