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# Microstructure and remarkably improved hydrogen storage properties of Mg<sub>2</sub>Ni alloys doped with metal elements of Al, Mn and Ti

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**Abstract:** Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> (M=Al, Mn and Ti) alloys were prepared by solid phase sintering process. The phases and microstructure of the alloys were systematically characterized by XRD, SEM and STEM. It was found that Mg<sub>3</sub>MNi<sub>2</sub> intermetallic compounds formed in Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys and coexisted with Mg and Mg<sub>2</sub>Ni, and that radius of M atoms closer to that of Mg atom was more beneficial to the formation of Mg<sub>3</sub>MNi<sub>2</sub>. The hydrogen storage properties and corrosion resistance of Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys were investigated through Sievert and Tafel methods. Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys exhibited remarkably improved hydrogen absorption and desorption properties. Significantly reduced apparent dehydriding activation energy values of -46.12, -59.16 and -73.15 kJ/mol were achieved for Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub>, Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> alloys, respectively. The corrosion potential of Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys shifted to the positive position compared with Mg<sub>2</sub>Ni alloy, e.g. there was a corrosion potential difference of 0.110 V between Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> alloy (-0.529 V) and Mg<sub>2</sub>Ni (-0.639 V), showing improved anti-corrosion properties by the addition of Al, Mn and Ti. **Key words:** Mg<sub>2</sub>Ni; Mg<sub>3</sub>MNi<sub>2</sub>; hydriding kinetics; dehydriding activation energy; anti-corrosion properties

# **1** Introduction

Mg-based alloys were regarded as a candidate of the most promising hydrogen storage materials [1]. Typically, Mg<sub>2</sub>Ni had been intensively investigated as a gaseous hydrogen storage alloy and negative electrode material of nickel-metal hydride (Ni-MH) battery [2]. As a hydrogen storage material, its sluggish kinetics should be improved, and the operation temperature needed to be lowered. Therefore, tremendous efforts had been devoted to investigate and improve the hydrogen storage properties of Mg<sub>2</sub>Ni. Ball milling and rapid quenching were widely used to fabricate amorphous/ nanocrystalline Mg<sub>2</sub>Ni for enhancing the hydrogen absorption and desorption [3]. Alternatively, novel synthetic techniques, such as hydriding combustion synthesis (HCS) and hydrogen plasma metal reaction technique, were developed to synthesize Mg<sub>2</sub>Ni for further improving the hydrogen absorption/desorption kinetics [4,5]. Furthermore, it was observed that the absorption/desorption kinetics of Mg2Ni could be significantly improved by doping with metals, such as V, Cr, Fe, Co and Cu [6]. For example, the hydrogen desorption activation energy of Mg<sub>2</sub>Ni was lowered to 50.50 kJ/mol by doping with La and Cu through rapid quenching [7]. Although encouraging progresses had been achieved by alloying, element substitution, nanocrystallization and so on [8–11], it still could not meet the requirements for on-board utilization.

On the other hand, Mg<sub>2</sub>Ni base alloys were regarded as one of the most promising negative electrode materials for Ni–MH battery due to the high theoretical capacity and low cost. However, the actual capacity of crystalline Mg<sub>2</sub>Ni alloy electrode was not so high as expected, and the cyclic property was very poor [12]. The amorphous Mg<sub>2</sub>Ni alloy obtained via ball milling showed superior discharge capacity [2]. While the amorphous Mg<sub>2</sub>Ni suffered from serious corrosion and most capacity was lost within several charge–discharge cycles [13,14]. So, enhancing anti-corrosion and improving cyclic stability were also imperative for the Mg<sub>2</sub>Ni-based alloy electrodes.

Doping metal elements was a traditional and

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effective way to improve the hydrogen storage properties of Mg-based alloys [15,16]. Interestingly, it has been recently reported that introducing some metals into Mg<sub>2</sub>Ni would form kinds of FCC-structure new ternary intermetallic compounds, such as Mg<sub>3</sub>MnNi<sub>2</sub>, Mg<sub>3</sub>AlNi<sub>2</sub>, Mg<sub>3</sub>TiNi<sub>2</sub> and Mg<sub>3</sub>GeNi<sub>2</sub>. Mg<sub>3</sub>AlNi<sub>2</sub>, Mg<sub>3</sub>TiNi<sub>2</sub> and Mg<sub>3</sub>MnNi<sub>2</sub> alloys were found readily absorbing/ desorbing hydrogen, and a new metal hydride Mg<sub>3</sub>MnNi<sub>2</sub>H<sub>3</sub> was observed [17,18]. Moreover, those ternary intermetallic compounds exhibited better electrochemical properties compared with the binary Mg<sub>2</sub>Ni alloy.

As well known, there were "synergetic or pump effects" during hydriding and dehydriding processes when Mg-based alloys composited with some readily hydrogen absorption/desorption alloys, such as AB<sub>5</sub> alloy [19]. However, it was still unknown whether and how Mg<sub>3</sub>MNi<sub>2</sub> would affect the hydrogen storage properties of Mg-based alloys. Herein, a series of alloys with nominal compositions of  $Mg_2Ni_{0.7}M_{0.3}$  (M = Al, Mn and Ti) were prepared. The phase component, phase structure and microstructure of the alloys were characterized by powder X-ray diffractometry (XRD), scanning electron microscopy (SEM) and scanning transmission electron microscopy (STEM). The hydrogen storage properties were systematically investigated by Sievert method, and the corrosion resistance performance was evaluated through Tafel As а consequence, Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub>, measurement. Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> and Mg<sub>2</sub>Ni<sub>0.7</sub>Ti<sub>0.3</sub> alloys exhibited significantly reduced apparent dehydriding activation energies (E<sub>a</sub>) of -46.12, -59.16 and -73.15 kJ/mol, respectively. A distinguishable reduction of dehydriding enthalpy was also observed for Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> alloy. The anti-corrosion properties of Mg2Ni07M03 alloy electrodes were also visibly improved compared with Mg<sub>2</sub>Ni alloy.

# 2 Experimental

 $Mg_2Ni_{0.7}M_{0.3}$  alloys were prepared by lowtemperature solid phase sintering method. Firstly, the designed individual metal powder mixtures were homogeneously mixed on a planetary ball mill (QM-3SP2, China), and then pressed into pieces followed by being sintered at 853 K for 6 h in a tube furnace with the protection of high purity argon. The purities of starting materials (Mg, Ni, Al, Mn and Ti powders, from Sinopharm Chemical Reagent Co., Ltd.) were all higher than 99.99%.

The phase analysis was performed by powder X-ray diffraction (XRD) on a Philips X'Pert diffractometer (PANalytical X'Pert MRD) with Cu K<sub> $\alpha$ </sub> radiation ( $\lambda$ = 1.54056 Å). Before starting the measurement, the zero shift of diffractometer system was calibrated by high

purity silicon (with a purity of 99.999%). The lattice constants were calculated by Rietveld method using the X'Pert high score plus software. The microstructure and phase distribution were observed by scanning electron microscopy (SEM, ZEISS EVO18) and scanning transmission electron microscopy (STEM, FEI TALOS F200S).

The hydriding/dehydriding kinetics and pressurecomposition isotherms (PCI) curves were measured by an automatic Sieverts apparatus (PCTPro E&E, SETARAM Inc., France). Before the experimental data collecting, 0.6000 g sample was fully activated by undergoing more than three cycles of hydrogen absorption/desorption at 573 K. The hydrogen absorption kinetics was measured under a starting pressure of 3 MPa. The hydrogen desorption kinetics was measured in nearly vacuum condition. The PCI measurements were carried out following the kinetics test. Finally, the Tafel curves were achieved using a standard test method on the instrument CHI660E (China).

### **3** Results and discussion

#### 3.1 Phase analysis and microstructure

Figure 1 showed the XRD patterns of the as-sintered Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys. It was obviously observed that the FCC-structure intermetallic compounds of Mg<sub>3</sub>AlNi<sub>2</sub>, Mg<sub>3</sub>MnNi<sub>2</sub> and Mg<sub>3</sub>TiNi<sub>2</sub> (summarized as Mg<sub>3</sub>MNi<sub>2</sub>) formed in each alloy. It was considered that the intermetallic Mg<sub>3</sub>MNi<sub>2</sub> compounds often coexisted with Mg when Mg<sub>2</sub>Ni doped with mental elements, such as Al, Mn and Ti. Thus, element Mg was found in all alloys. For Mg<sub>2</sub>Ni<sub>0.7</sub>Ti<sub>0.3</sub> alloy, the amount of element Mg was even more than that of Mg<sub>2</sub>Ni as judged by the intensity of the XRD peaks shown in Fig. 1(c). It could be found that the formation of intermetallic Mg<sub>3</sub>TiNi<sub>2</sub> compound was difficult due to the large difference of atomic radius between Ti (2.00 Å) and Mg (1.72 Å), and the strong affinity of Ti and Ni led to the formation of Ni<sub>3</sub>Ti. It was reported that the lattice sites of Mg (6i) in Mg<sub>2</sub>Ni unit cell were replaced by three Mn atoms, resulting in the formation of cubic structure Mg9Mn3Mg(6i)Ni6 compounds (normally written as Mg\_3MnNi\_2) [20,21]. Since Mg\_3TiNi\_2 was similar with Mg<sub>3</sub>MnNi<sub>2</sub> in crystal structure, it could be naturally inferred that the difficulty of formation of Mg<sub>3</sub>TiNi<sub>2</sub> was attributed to the large atomic radius of Ti. Based on Fig. 1, the lattice constants of Mg<sub>3</sub>AlNi<sub>2</sub>, Mg<sub>3</sub>MnNi<sub>2</sub> and  $Mg_3TiNi_2$  were calculated to be 1.1539(7), 1.1581(8) and 1.1617(6) nm, respectively. It was obvious that Mg<sub>3</sub>TiNi<sub>2</sub> had the largest lattice constant. The stability of intermetallic Mg<sub>3</sub>MNi<sub>2</sub> compounds could be related with the doped elements M. For example, ZHANG et al [21] reported that the stability of Mg<sub>3</sub>AlNi<sub>2</sub> was the highest

among those intermetallic compounds. This was consistent with the present results, i.e.  $Mg_3TiNi_2$  was more difficult to form than  $Mg_3MnNi_2$  and  $Mg_3AlNi_2$ . So, it could be concluded that metal elements M with similar atomic radii to Mg were more beneficial to the formation and stability of intermetallic  $Mg_3MNi_2$  compounds for the lower lattice distortion energy. Obviously,  $Mg_3TiNi_2$  had the lowest stability among the intermetallic  $Mg_3MNi_2$  compounds due to its high lattice distortion energy resulting from the largest Ti atomic radium. As a consequence, only small amount of  $Mg_3TiNi_2$  was found in the  $Mg_2Ni_{0.7}Ti_{0.3}$  alloy.



Fig. 1 Typical XRD patterns of sintered  $Mg_2Ni_{0.7}M_{0.3}$  alloys: (a)  $Mg_2Ni_{0.7}Al_{0.3}$ ; (b)  $Mg_2Ni_{0.7}Mn_{0.3}$ ; (c)  $Mg_2Ni_{0.7}Ti_{0.3}$ 

To explore the phase transition, the hydrogenated/ dehydrogenated Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> alloys were subjected to powder XRD measurement, and the results were illustrated in Fig. 2. Figure 2(a) showed the XRD pattern of Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> alloy hydrogenated at 553 K, in which Mg<sub>3</sub>AlNi<sub>2</sub>, Mg<sub>2</sub>NiH<sub>4</sub>, Mg<sub>2</sub>NiH<sub>0.3</sub> and MgO were identified. Because this sample was exposed to the open air for a long period, the elemental Mg was oxidized to MgO. Thus, MgH<sub>2</sub> was not found in the sample. This result also indicated that Mg2Ni and Mg3AlNi2 were stable in the open air. The hydride of Mg<sub>3</sub>AlNi<sub>2</sub>H<sub>3</sub> was not found in the sample because of the over high hydriding temperature [18]. However, the solid solution of Mg<sub>2</sub>NiH<sub>0.3</sub> was observed, which could form from dehydrogenation of Mg<sub>2</sub>NiH<sub>4</sub> in cooling process. Figure 2(b) showed the XRD pattern of the dehydrogenated Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> alloy (not exposed to air). Obviously, the original phase components (Mg<sub>2</sub>Ni, Mg<sub>3</sub>AlNi<sub>2</sub> and Mg, Fig. 1(a)) were recovered from dehydrogenation, indicating a reversible phase transition upon hydriding and dehydriding for Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> alloy. That was to say, the hydrogenation of Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> alloy was fully reversible. The phase transition of Mg2Ni0.7Mn0.3 and Mg2Ni0.7Ti0.3 alloys was similar to that of Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> alloy.



Fig. 2 Typical XRD patterns of  $Mg_2Ni_{0.7}Al_{0.3}$  alloys: (a) As-hydrogenated at 553 K (stored in open air); (b) Asdehydrogenated (stored in glovebox)

Figure 3 showed the SEM and STEM images of  $Mg_2Ni_{0.7}Al_{0.3}$  alloy. The backscattered electron image (Fig. 3(a)) illustrated that  $Mg_3AlNi_2$  particles (marked with arrows) were embedded in the matrix of Mg and  $Mg_2Ni$  with a dimension of several micrometers. Mg and  $Mg_2Ni$  could not be distinguished by the back-



Fig. 3 SEM (a) and STEM (b) images of Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> alloy

scattered electron. For further investigating the microstructure, the electron diffraction was also performed and the results were illustrated in Fig. 3(b). The high-resolution lattice image combining the electron diffraction pattern indicated that Mg<sub>3</sub>AlNi<sub>2</sub> was of a nanograin structure. Actually, the large particles of Mg<sub>3</sub>AlNi<sub>2</sub>, observed in Fig. 3(a), contained lots of nanograins. On the other hand, the grain boundaries between the Mg<sub>3</sub>AlNi<sub>2</sub> and Mg<sub>2</sub>Ni (or Mg) phases were not clear, showing a transitional layer with several atomic thicknesses. This special microstructure was possibly related to the formation mechanism of Mg<sub>3</sub>AlNi<sub>2</sub>. It was thought that three Al atoms substituted three Mg(6i) lattice sites in the Mg<sub>2</sub>Ni unit cell, forming a cubic structure Mg<sub>9</sub>Al<sub>3Mg(6i)</sub>Ni<sub>6</sub> [20]. This formation mechanism could also explain why Mg<sub>3</sub>AlNi<sub>2</sub> always coexisted with the elemental Mg in Mg2Ni0.7Al0.3 alloy, as observed in Fig. 1(a).

#### 3.2 Hydrogen storage properties

The rates of hydrogen absorption at different temperatures for Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub>, Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> and Mg<sub>2</sub>Ni<sub>0.7</sub>Ti<sub>0.3</sub> alloys were measured and shown in Figs. 4(a)–(c), respectively. It could be observed that the Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys all had fairly good hydrogen absorption kinetics. The hydrogen absorption of Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys was all almost completed in 300 s at a low temperature of 493 K under a starting hydrogen pressure of 3 MPa. The hydriding kinetics of Mg<sub>2</sub>Ni<sub>07</sub>M<sub>03</sub> alloys was remarkably improved compared with pure Mg or Mg<sub>2</sub>Ni [7,22], which could be related to the intermetallic compounds of Mg<sub>3</sub>MNi<sub>2</sub>. Although hydrides of Mg<sub>3</sub>MNi<sub>2</sub>H<sub>3</sub> were not found in the present experiments, it was reported that H atoms could dissolve in the octahedral and tetrahedral interstices in the lattice of Mg<sub>3</sub>MnNi<sub>2</sub> [18]. However, the decomposition of H<sub>2</sub> molecules to H atoms was exactly a key barrier to block the quick hydrogen absorption of Mg-based alloys [23]. In fact, the PCI results indicated that Mg<sub>3</sub>MNi<sub>2</sub> absorbed a small amount of hydrogen (about 0.3%, mass fraction). It was reasonably considered that H<sub>2</sub> molecules were firstly decomposed to H atoms and dissolved in the intermetallic Mg<sub>3</sub>MNi<sub>2</sub> compounds, and then the H atoms transferred to Mg and Mg2Ni, forming metal hydrides (MgH<sub>2</sub> and Mg<sub>2</sub>NiH<sub>4</sub>). Thus, the hydriding kinetics of Mg and Mg<sub>2</sub>Ni was remarkably improved. Certainly, the nanograin structure and the phase boundaries also benefited to the improvement of hydrogen absorption, which was confirmed in many hydrogen storage material systems [16,22]. From Fig. 4, it could be also observed that the temperature did not significantly affect the hydrogen absorption rate when the hydriding temperature was higher than 493 K.

For practical utilization, it was confronted with a

great challenge to improve the dehydriding kinetics. Accordingly, the dehydriding properties of  $Mg_2Ni_{0.7}M_{0.3}$  alloys were systematically investigated. Figure 5 showed the dehydriding curves of  $Mg_2Ni_{0.7}M_{0.3}$  alloys at different temperatures. It should be pointed out that  $Mg_2Ni_{0.7}Al_{0.3}$  alloy did not complete hydrogen desorption at 493 and 513 K for dehydrogenation reaching equilibrium. The released hydrogen increased with the increase of dehydrding temperature due to the higher equilibrium pressure, and the hydrogen desorption rates were observably accelerated at the same time.



Fig. 4 Hydriding kinetics of  $Mg_2Ni_{0.7}Al_{0.3}(a)$ ,  $Mg_2Ni_{0.7}Mn_{0.3}(b)$ and  $Mg_2Ni_{0.7}Ti_{0.3}(c)$ 



Fig. 5 Dehydriding curves of  $Mg_2Ni_{0.7}Al_{0.3}$  (a),  $Mg_2Ni_{0.7}Mn_{0.3}$  (b) and  $Mg_2Ni_{0.7}Ti_{0.3}$  (c)

Figure 6 illustrated the Arrhenius plots for the dehydrogenation of  $Mg_2Ni_{0.7}M_{0.3}$  alloys. The Arrhenius equation could be written as

$$K = K_0 \exp[-E_a/(RT)] \tag{1}$$

where K is the dehydriding reaction constant, which could be achieved by fitting the starting linear part of the hydrogen desorption curves (Fig. 5) using the Johnson– Mehl–Avrami–Kolmogorov (JMAK) equation; R is the mole gas constant; T is the hydrogen desorption temperature;  $E_a$  is the the apparent activation energy of dehydrogenation. By this method,  $E_a$  values were gotten to be -46.12, -59.16 and -73.15 kJ/mol for Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub>, Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> and Mg<sub>2</sub>Ni<sub>0.7</sub>Ti<sub>0.3</sub> alloys, respectively, which were all far smaller than our previous reported values [24], and the recently reported values for Mg-based alloys [25].



Fig. 6 Arrhenius plots for dehydrogenation of  $Mg_2Ni_{0.7}M_{0.3}$  alloys

The high thermodynamic stability of hydrides was another critical challenge for Mg-based hydrogen storage materials. Thus, the thermodynamic destabilization of hydrides was a very crucial issue for hydrogen storage materials. Figure 7(a) showed the PCI curves of Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> alloy at different temperatures. Observably, there were two plateaus respectively corresponding to the hydrogen absorption and desorption of Mg (marked as Plat. 1) and Mg<sub>2</sub>Ni (marked as Plat. 2). The hydriding/dehydriding plateaus of Mg<sub>3</sub>MnNi<sub>2</sub> did not exhibit in the PCI curves. This could be inferred that Mg<sub>3</sub>MnNi<sub>2</sub> did not absorb hydrogen to transform to Mg<sub>3</sub>MnNi<sub>2</sub>H<sub>3</sub> at the studied temperatures because Mg<sub>3</sub>MnNi<sub>2</sub>H<sub>3</sub> was a room temperature stable hydride. This was consistent with the above XRD phase analysis. However, as observed in Figs. 7(a) and (b), Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> and Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> alloys absorbed about 0.3% H<sub>2</sub> (mass fraction) when the pressure was higher than the Plat. 2. This capacity (0.3%) could be attributed to the dissolution of H atoms in the lattice interstice of  $Mg_2Ni_{0.7}Mn_{0.3}$  and  $Mg_3MnNi_2$ , which could be confirmed by Fig. 7(b). Figure 7(b) illustrated the comparison of PCI curves for  $Mg_2Ni_{0.7}Al_{0.3}$ , Mg<sub>2</sub>Ni<sub>07</sub>Mn<sub>03</sub> and Mg<sub>2</sub>Ni<sub>07</sub>Ti<sub>03</sub> alloys at the same temperature of 533 K. The hydrogen capacity reduced with the increase of a mount of Mg<sub>3</sub>MNi<sub>2</sub> in the alloys. For Mg<sub>2</sub>Ni<sub>0.7</sub>Ti<sub>0.3</sub> alloy, the capacity was the highest due to a trace of Mg<sub>3</sub>TiNi<sub>2</sub> in the alloy. Unlike Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> and Mg2Ni0.7Mn0.3 alloys, Mg2Ni0.7Ti0.3 alloy had no obvious increase of capacity when the pressure was higher than Plat. 2. On the other hand, the hydriding/dehydriding plateau pressure of Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub>

alloys increased a little due to the introduction of  $Mg_3MNi_2$ .



Fig. 7 PCI curves of  $Mg_2Ni_{0.7}Mn_{0.3}$  alloys at different temperatures (a) and comparison of PCI curves of  $Mg_2Ni_{0.7}M_{0.3}$  alloys at 533 K (b)

The hydriding/dehydriding thermodynamic properties were often evaluated by the hydriding/ dehydriding enthalpy ( $\Delta H$ ) and entropy ( $\Delta S$ ), which could be calculated by vant' Hoff equation as follows:

$$\ln\left(\frac{p_{\rm eq}}{p_0}\right) = \frac{\Delta H}{RT} - \frac{\Delta S}{R} \tag{2}$$

where  $p_{eq}$  and  $p_0$  represent the equilibrium pressure and the standard atmospheric pressure, respectively. In this calculation, the equilibrium pressures  $(p_{eq})$  were taken from the midpoint at the hydrogen desorption plateaus of Mg and Mg<sub>2</sub>Ni in Fig. 7(a). The vant' Hoff plots for the dehydrogenation of Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> alloy were illustrated in Fig. 8. The calculated enthalpies were (74.12±0.62) and (62.9±0.06) kJ/mol for Mg and Mg<sub>2</sub>Ni, respectively, and the corresponding entropies were (135.45±1.91) and (120.91±0.12) J/(mol·K). The enthalpies had a distinguishable change compared with previous reported values for Mg (77.9 kJ/mol) [22] and Mg<sub>2</sub>Ni (64.6 kJ/mol) [26]. The possible reasons for the reduction of dehydriding enthalpies could be attributed to the synergistic dehydriding effects among Mg, Mg<sub>2</sub>Ni

and Mg<sub>3</sub>MnNi<sub>2</sub>, as it was reported that Mg<sub>2</sub>NiH<sub>0.3</sub> could enhance dehydriding of MgH<sub>2</sub> [27]. In fact, Mg<sub>2</sub>NiH<sub>0.3</sub> could serve as a "hydrogen pump" for the dehydrogenation of MgH<sub>2</sub>. As discussed above, the H atoms could also dissolve in the lattice of Mg<sub>3</sub>MnNi<sub>2</sub>. So, it could be inferred that Mg<sub>3</sub>MnNi<sub>2</sub> could also have a similar effect with Mg<sub>2</sub>NiH<sub>0.3</sub> on promoting hydrogen desorption of MgH<sub>2</sub> and Mg<sub>2</sub>NiH<sub>4</sub>. On the other hand, there were reports that the intermixed region and interfacial free energy could destabilize the hydrides [28]. Obviously, there were interfacial free energy and large amount of intermixed regions in Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> alloy due to its nanograin microstructure. At last, the lattice elastic stress resulting from dehydrogenation could also have the destabilized effect on the adjacent hydrides [29]. Accordingly, a reduction of dehydriding enthalpies for MgH<sub>2</sub> and Mg<sub>2</sub>NiH<sub>4</sub> was achieved upon Mg<sub>2</sub>Ni<sub>0.7</sub>Mn<sub>0.3</sub> alloy.



Fig. 8 Vant' Hoff plots for hydrogen desorption of Mg and  $Mg_2Ni$ 

#### 3.3 Corrosion resistance performance

As a promising electrode material of Ni-MH battery, it was also very important to improve the corrosion resistance of the Mg-based alloy in alkaline electrolyte [30,31]. Thus, the Tafel polarization curves of Mg<sub>2</sub>Ni and Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloy electrodes were measured and illustrated in Fig. 9. The electrochemical parameters related to corrosion (equilibrium potential  $\varphi_{corr}$ , linear polarization resistance  $R_p$  and corrosion current  $J_{corr}$ ) were achieved by fitting the polarization cures (Fig. 9) and summarized in Table 1. Visibly, Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys had better corrosion resistance properties than Mg<sub>2</sub>Ni alloy judging from  $J_{corr}$ . Compared with Mg<sub>2</sub>Ni, the  $\varphi_{corr}$ of Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys shifted to the positive position, for example, there was a difference of 0.110 V between  $\varphi_{corr}$  values of Mg<sub>2</sub>Ni<sub>0.7</sub>Al<sub>0.3</sub> alloy (-0.529 V (vs SCE)) and Mg<sub>2</sub>Ni (-0.639 V (vs SCE)), also indicating an improvement of corrosion resistance due to the addition of M elements. It was found that Mg<sub>3</sub>MnNi<sub>2</sub> phase could

enhance the anti-corrosive performance of the particle surface of Mg<sub>2</sub>Ni alloys [32]. In this work, the movement of  $\varphi_{corr}$  could be attributed to the introduction of Mg<sub>3</sub>MNi<sub>2</sub> phases in the Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloys. And there was another interesting phenomenon that the  $R_p$  of Mg<sub>2</sub>Ni<sub>0.7</sub>Ti<sub>0.3</sub> alloy was the highest among the Mg<sub>2</sub>Ni<sub>0.7</sub>M<sub>0.3</sub> alloy electrodes. It was reported that Mg<sub>3</sub>MNi<sub>2</sub> could enhance the reaction activity and lower the pulverization rate of particles [32–34]. There was a trace of Mg<sub>3</sub>TiNi<sub>2</sub> phase in the Mg<sub>2</sub>Ni<sub>0.7</sub>Ti<sub>0.3</sub> alloy, and it was thought that Mg<sub>2</sub>Ni<sub>0.7</sub>Ti<sub>0.3</sub> alloy had the maximum amount of Mg, thus leading to a thicker layer of Mg(OH)<sub>2</sub> covered on the electrode, which could block the movement of electrons. As a result, Mg<sub>2</sub>Ni<sub>0.7</sub>Ti<sub>0.3</sub> alloy showed a high  $R_p$ .



Fig. 9 Tafel polarization curves of  $Mg_2Ni$  and  $Mg_2Ni_{0.7}M_{0.3}$  electrodes

 Table 1 Electrochemical parameters related to corrosion

Sample	$\varphi_{\rm corr}$ (vs SCE)/V	$R_{\rm p}/(\Omega \cdot {\rm g}^{-1})$	$J_{\rm corr}/(\mu {\rm A} \cdot {\rm g}^{-1})$
Mg <sub>2</sub> Ni	-0.639	220	0.0472
$Mg_2Ni_{0.7}Ti_{0.3}$	-0.548	749	0.0242
$Mg_2Ni_{0.7}Al_{0.3}$	-0.529	354	0.0275
$Mg_2Ni_{0.7}Mn_{0.3}$	-0.579	287	0.0316

# **4** Conclusions

1) The FCC-structure intermetallic  $Mg_3MNi_2$  compounds formed in  $Mg_2Ni_{0.7}M_{0.3}$  (M = Al, Mn and Ti) alloys, and M element with atomic radius closer to Mg was more favorable to the formation of  $Mg_3MNi_2$ . H atoms could dissolve in the intermetallic  $Mg_3MNi_2$  compounds forming solid solutions.

2) The intermetallic  $Mg_3MNi_2$  compounds could accelerate the hydrogen adsorption and desorption of Mg-based alloys. The apparent activation energies of dehydrogenation reduced to be -46.12, -59.16 and -73.15 kJ/mol for  $Mg_2Ni_{0.7}Al_{0.3}$ ,  $Mg_2Ni_{0.7}Mn_{0.3}$  and

 $Mg_2Ni_{0.7}Ti_{0.3}$  alloys, respectively. And there was also a distinguishable reduction in dehydriding enthalpy for  $Mg_2Ni_{0.7}M_{0.3}$  alloy.

3)  $Mg_3MNi_2$  phase had positive effects on the improvement of anti-corrosion performances for  $Mg_2Ni_{0.7}M_{0.3}$  alloys.

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# 添加金属元素 Al、Mn 和 Ti 后 Mg<sub>2</sub>Ni 合金的 显微组织及其显著改善的储氢性能

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摘 要:采用固相烧结方法制备  $M_{g_2}N_{i_0,7}M_{0,3}$  (M = Al, Mn, Ti)合金。利用 X 射线衍射仪、扫描电镜和扫描透射电 镜对合金的相组成和显微组织进行系统表征。结果发现, $M_{g_2}N_{i_0,7}M_{0,3}$  合金中形成了具有面心立方结构的金属间 化合物  $M_{g_3}MN_{i_2}$ ,其与 Mg 和  $M_{g_2}N_{i}$  共存;且 M 原子半径与 Mg 原子半径越接近,越有利于  $M_{g_3}MN_{i_2}$ 的形成。 采用 Sievert 和 Tafel 方法对  $M_{g_2}N_{i_0,7}M_{0,3}$  合金的储氢性能和耐腐蚀性能进行研究。 $M_{g_2}N_{i_0,7}M_{0,3}$  合金的吸/放氢性能 得到明显改善。 $M_{g_2}N_{i_0,7}Al_{0,3}$ , $M_{g_2}N_{i_0,7}M_{0,3}$  和  $M_{g_2}N_{i_0,7}T_{i_0,3}$  合金的脱氢反应的激活能较  $M_{g_2}N_{i}$  的激活能明显降低, 分别为-46.12、-59.16和-73.15 kJ/mol。与 $M_{g_2}N_{i}$  合金相比, $M_{g_2}N_{i_0,7}M_{0,3}$  合金的腐蚀电位向正方向移动,如  $M_{g_2}N_{i_0,7}Al_{0,3}$  合金(-0.529 V)与  $M_{g_2}N_{i}$  合金(-0.639 V)的腐蚀电位差为 0.110 V,表明添加 Al、Mn 和 Ti 能使合金的 耐腐蚀性能得到显著提高。

关键词: Mg<sub>2</sub>Ni; Mg<sub>3</sub>MNi<sub>2</sub>; 吸氢动力学; 脱氢激活能; 耐腐蚀性能