

MICROSTRUCTURE AND J_c OF Y-Ba-Cu-O SUPERCONDUCTOR AFTER P_{O_2} -ALTERNATIVE HEAT TREATMENT^①

Chen, Kanghua Huang, Peiyun
Powder Metallurgy Research Institute,
Central South University of Technology, Changsha 410083

ABSTRACT The effect of P_{O_2} -alternative heat treatment on the melting point, the microstructure and the J_c of $YBa_2Cu_3O_{7-\delta}$ superconductor has been investigated. It is found that the melting point of $YBa_2Cu_3O_{7-\delta}$ decreased to 900 °C when P_{O_2} decreased to 10 Pa. The texture of the $YBa_2Cu_3O_{7-\delta}$ polycrystal could occur at temperatures lower than 920 °C after P_{O_2} -alternative treatment.

Key words: ceramic superconductor $YBa_2Cu_3O_{7-\delta}$ preparation texture

1 INTRODUCTION

It is necessary to produce ceramic superconductor in available shapes, such as wire or tape for their applications. $YBa_2Cu_3O_{7-\delta}$ superconducting wire or tape can be easily fabricated by means of powder-in-tube technology, or drawing and rolling of $YBa_2Cu_3O_{7-\delta}$ powder sheathed with Ag tube^[1]. However, critical current density of sintered $YBa_2Cu_3O_{7-\delta}$ tape or wire would deteriorate rapidly in weak magnetic field. Since the melting temperature of Ag is lower than that of $YBa_2Cu_3O_{7-\delta}$ in air, Ag-sheathed $YBa_2Cu_3O_{7-\delta}$ tape or wire can only endure sintering and not endure melt-crystallizing in air. Some available heat treatments should be developed to improve the field dependence of the critical current density of Ag-sheathed $YBa_2Cu_3O_{7-\delta}$ wire or tape. Based on the fact that the stability of $YBa_2Cu_3O_{7-\delta}$ depends on not only temperature but also P_{O_2} ^[2], the compacted $YBa_2Cu_3O_{7-\delta}$ pellets were heat-treated in a P_{O_2} -alternative atmosphere to search that the $YBa_2Cu_3O_{7-\delta}$ could melt and crystallize at a temperature

lower than the melting temperature of Ag.

2 EXPERIMENTAL

2.1 Melting Examination of the $YBa_2Cu_3O_{7-\delta}$

$YBa_2Cu_3O_{7-\delta}$ powder was prepared by chemical reaction of solid state. The powder was treated at various temperatures and P_{O_2} . The treated powder was characterized by XRD to examine the decomposition of the $YBa_2Cu_3O_{7-\delta}$. Whether $YBa_2Cu_3O_{7-\delta}$ melts or not in the treatments was determined according to the adhesive strength between the particles in the treated powder. Furthermore, the rolled thick film of $YBa_2Cu_3O_{7-\delta}$ powder with Ag substrate was examined before and after melting treatment. In the present experiments, P_{O_2} was adjusted by the pressure of flowing air through the tube furnace.

2.2 P_{O_2} -alternative Treatment of $YBa_2Cu_3O_{7-\delta}$ Pellet

$YBa_2Cu_3O_{7-\delta}$ powder was compacted into

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pellets of d 10 mm \times 0.1 mm at 2.5 GPa. The pellets were treated for 0.1 ~ 1 h at 850 ~ 920 °C and 1 ~ 100 Pa P_{O_2} , then held for 2 h at 850 ~ 920 °C and 0.1 MPa P_{O_2} . After cooled in furnace, the critical current densities of the treated pellets were measured in magnetic field by four-probe DC method with the criterion of 1 μ V/cm, and their microstructures were characterized by SEM.

3 RESULTS AND DISCUSSION

Fig. 1 shows the results of the melting (decomposing) of $YBa_2Cu_3O_{7-x}$. It can be seen that $YBa_2Cu_3O_{7-x}$ would melt at a temperature lower than 920 °C under 20 Pa oxygen pressure. The surface of the $YBa_2Cu_3O_{7-x}$ thick film treated under the above condition exhibits molten status, as shown in Fig. 2. This result is inconsistent with Lay *et al.*^[3] who reported that $YBa_2Cu_3O_{7-x}$ would start to decompose at higher temperature under the same P_{O_2} in DTA study. $YBa_2Cu_3O_{7-x}$ is rather stable, as shown in Fig. 3. In Lay's DTA, the rate of temperature rising was 10 °C/min and there was no duration at the measured temperature. It suggests that the difference in the decomposing or melting point of $YBa_2Cu_3O_{7-x}$ between the present study and the Lay's rises from the hysteresis of decomposing of $YBa_2Cu_3O_{7-x}$

measured in DTA. It is obvious from Fig. 1 that the effect of P_{O_2} is similar to that of temperature for $YBa_2Cu_3O_{7-x}$. The microstructure evolution of $YBa_2Cu_3O_{7-x}$ pellets in P_{O_2} -alternative treatment was shown in Fig. 4. After P_{O_2} -low treatment, $YBa_2Cu_3O_{7-x}$ pellet exhibits a

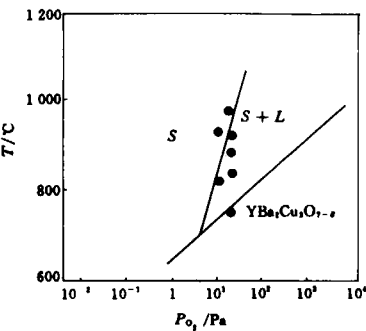


Fig. 1 The dependence of the melting (decomposing) point of $YBa_2Cu_3O_{7-x}$ on P_{O_2} , solid circles represent the experimental conditions of P_{O_2} -temperature, L and S represent solid phase and liquid phase respectively

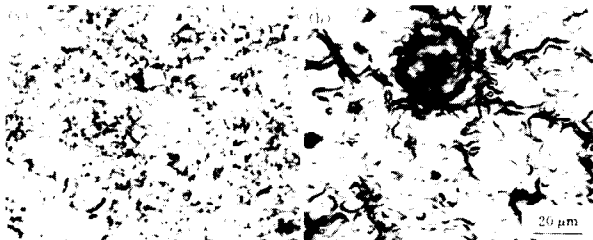


Fig. 2 The surface microstructures of the rolled thick films of $YBa_2Cu_3O_{7-x}$ powder with Ag substrate. The films treated at 900 °C for 0.5 h at (a) 0.1 MPa P_{O_2} , (b) 20 Pa P_{O_2}

dense and homogeneous microstructure, yet $\text{YBa}_2\text{Cu}_3\text{O}_{7-x}$ pellet treated at alternative P_{O_2} exhibits a locally-textured microstructure which is similar to that of melt-texture growth reported by Jin^[4]. The mechanism of the microstructural evolution can be suggested as follows. In the P_{O_2} -alternative treatment, $\text{YBa}_2\text{Cu}_3\text{O}_{7-x}$ would melt in P_{O_2} -low treatment, then $\text{YBa}_2\text{Cu}_3\text{O}_{7-x}$ grains preferentially grow in the liquid state under P_{O_2} -high treatment. In other words, the mechanism is similar to the melt-texture growth reported by

Salama *et al.*^[5].

The improved microstructure of the $\text{YBa}_2\text{Cu}_3\text{O}_{7-x}$ pellet treated in P_{O_2} -alternative atmosphere is responsible for the reduced field dependence of the J_c , as shown in Fig. 5. The J_c value of the sintered $\text{YBa}_2\text{Cu}_3\text{O}_{7-x}$ deteriorates exponentially in weak magnetic fields. On the contrary, J_c of the $\text{YBa}_2\text{Cu}_3\text{O}_{7-x}$ Pellet treated at alternative P_{O_2} is hardly affected by weak magnetic fields.

The microstructural evolution mentioned above and the J_c improvement of $\text{YBa}_2\text{Cu}_3\text{O}_{7-x}$

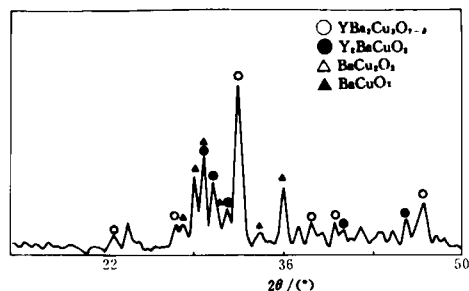


Fig. 3 The X-ray diffraction pattern of $\text{YBa}_2\text{Cu}_3\text{O}_{7-x}$ powder compact treated at 910 °C for 1 h at 20 Pa P_{O_2}

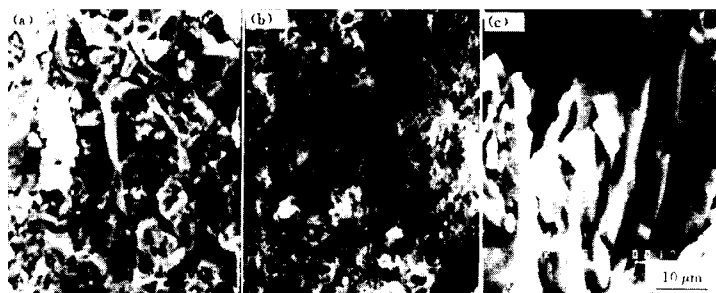


Fig. 4 The microstructure of $\text{YBa}_2\text{Cu}_3\text{O}_{7-x}$ pellets ($\times 1560$)
(a)—untreated; (b)—treated at 900 °C and 20 Pa P_{O_2} ;
(c)—treated at 20 Pa P_{O_2} and retreated at 0.1 MPa P_{O_2} at 900 °C

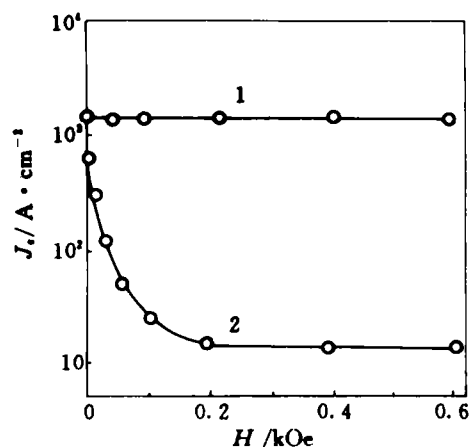


Fig. 5 The dependence of the J_c (77 K) of Y-Ba-Cu-O superconductor on magnetic field
(1)— P_{O_2} -alternatively treated; (2)—sintered

polycrystalline after P_{O_2} -alternative treatment show that the oxygen pressure can be controlled to decrease the temperature of melt-texture growth and improve the properties of

$YBa_2Cu_3O_{7-\delta}$ superconductor.

4 CONCLUSION

The melting temperature of $YBa_2Cu_3O_{7-\delta}$ can be decreased by controlling P_{O_2} in the atmosphere. The P_{O_2} -alternative treatment would result in melt-growth of $YBa_2Cu_3O_{7-\delta}$ at a temperature lower than 920 °C, and improve the field dependence of J_c .

REFERENCES

- 1 Yamada, Y *et al.* Jpn J Appl Phys, 1987, 26: L865.
- 2 Bormann, R; Nolting, J. Appl Phys Lett, 1989, 54: 2148.
- 3 Lay, K W; Renlund, G M. J Am Ceram Soc, 1990, 73: 1208.
- 4 Jin, S; Tiefel, T H *et al.* Phys Rev B, 1988, 37: 850.
- 5 Salama, K; Selvamanikam, V *et al.* Appl Phys Lett, 1989, 54: 2352.
- 9 Hattersley, B; Hume-Rothery, W. J Iron Steel Inst, 1966, 204: 683—701.
- 10 Barcik, J; Brzycka, B. Met Sci, 1983, 17: 256—260.
- 11 Maehara, Y; Ohmori, Y; Murayama, J; Fujino, N; Kunitake, T. Met Sci, 1983, 17: 541—547.
- 12 Rivlin, V G; Raynor, G V. Inter Met Rev, 1980, 25: 21—38.
- 13 Hillert, M; Qiu, C. Metall Trans A, 1990, 21A: 1673—1680.
- 14 Andersson, J O. PhD Thesis, Royal Inst of Technol, Stockholm, Sweden, 1986.
- 15 Frisk, K. PhD Thesis, Royal Inst of Technol, Stockholm, Sweden, 1990.
- 16 Andersson, J O; Sundman, B. CALPHAD, 1987, 11: 83—92.
- 17 Fernandez Guillermet, A. Bull Alloy Phase diagrams, 1982, 3: 359—367.
- 18 Li, J; Wu, T; Riquier, Y. Mater Sci Eng A, 1994, A174: 149—156.
- 19 Hosoi, Y. In: Proceedings of Stainless Steels'91, Chiba, Japan, Iron & Steel Inst of Japan. June 10—13, 1991.
- 20 Qiu, C. Metall Trans A, 1993, 24A: 2393—2409.
- 1 Schafmeister, V P; Ergang, R. Arch Eisenhüttenwes, 1939, 12: 459—464.
- 2 Rees, W P; Burns, B D; Cook, A J. J Iron Steel Inst, 1949, 162: 325—336.
- 3 Cook, A J; Brown, B R. J Iron Steel Inst, 1952, 171: 345—353.
- 4 Bradley, A J; Goldschmidt, H J. J Iron Steel Inst, 1941, 144: 273—288.
- 5 Nicholson, M E; Samans, C H; Shortsleeve, F J. Trans ASM, 1952, 44: 601—620.
- 6 Talbot, A M; Furman, D E. Trans ASM, 1953, 45: 429—442.
- 7 Lismer, R E; Pryce, L; Andrews, K W. J Iron Steel Inst, 1952, 171: 49—58.
- 8 Jones, J D; Hume-Rothery, W. J Iron Steel Inst 1966, 204: 1—7.