

# Simulation of microstructures in solidification of aluminum twin-roll casting

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**Abstract:** Based on the research on the solidification of twin-roll continuous casting aluminum thin strip, the analytical model of heterogeneous nucleation, the growth kinetics of tip (KGT) and columnar dendrite transformation to equiaxed dendrite (CET) of twin-roll continuous casting aluminum thin strip solidification was established by means of the principle of metal solidification and modern computer emulational technology. Meantime, based on the cellular automaton, the emulational model of twin-roll continuous casting aluminum thin strip solidification was established. The foundation for the emulational simulation of twin-roll casting thin strip solidification structure was laid. Meanwhile, the mathematical simulation feasibility was confirmed by using the solidification process of twin-roll continuous casting aluminum thin strip.

**Key words:** twin-roll continuous casting; solidification structure; emulational simulation; micro-model

## 1 Introduction

The twin-roll continuous casting thin strip is regarded as the most prospective technology of near-net-shape casting. Twin-roll strip continuous casting may save energy and manufacturing cost by eliminating some of the intermediate stages [1–7]. Furthermore, it can produce good properties due to high cooling rate.

Previous investigations [3] indicated that the solidification structure of twin-roll continuously cast thin strip, especially the crystal zone proportion, has an obvious effect on the thin strip quality. The control of the grain structure is of primary importance in twin-roll continuous cast strip because the solidification microstructure has a great influence on the quality and mechanical properties of strips. The microstructures of thin strip depend on the casting process parameters, and the microstructure has a great impact on its properties [8–11]. It is very necessary to investigate the effects of processing factors on the solidification structure zone of twin-roll continuously cast thin strips, such as pouring temperature, casting velocity and molten pool height. Considering that the matching degree among processing

factors of twin-roll continuous casting is very complex, if experimental method is used to investigate the effects, the expense and work load are very high. Oppositely, if numerical simulation method is adopted, the expense and work load are relatively low.

In this study, a simple micro mathematical model was performed to simulate the solidification structure of twin-roll continuously cast thin strip. Then the influence of the casting conditions on the micro structure in solidification of strip was investigated in detail. Based on the micro mathematical model, the average grain size and the average columnar crystal deviation for twin-roll continuously cast aluminum thin strip are investigated and analyzed.

## 2 Microscopic model

### 2.1 Nucleation model

The continuous nucleation model [12] is employed in the present study, based on the following assumptions: 1) the fragmentation of dendrites and the oxidation of melt surface are neglected; 2) the effect of convection on nucleation is not considered. In the model, the density of grains,  $n(\Delta T)$ , formed at any undercooling  $\Delta T$ , is

given by:

$$n(\Delta T) = \int_0^{\Delta T} \frac{n_{\max}}{\sqrt{2\pi}\Delta T_{\sigma}} \exp\left[-\frac{1}{2}\left(\frac{\Delta T - \Delta T_N}{\Delta T_{\sigma}}\right)^2\right] d(\Delta T) \quad (1)$$

where  $\Delta T_N$  is the mean nucleation undercooling;  $\Delta T_{\sigma}$  is the standard deviation; and  $n_{\max}$  is the maximum density of nuclei.

## 2.2 Growth kinetics model

In general, the constrained dendrite tip growth during rapid solidification was described by the Kurz-Giovanola-Trivedi (KGT) model [13]. However, it is well known that the twin-roll casting is a near-rapid solidification process thus the dendrite growth rate is not very high, and the growth dynamics coefficient is very large. Therefore, it is necessary to modify the model according to the solidification characteristics of twin-roll continuous cast thin strip. The modified KGT model is given as:

$$v_{\text{tip}} = \alpha(\Delta T)^2 + \beta(\Delta T)^3 \quad (2)$$

where  $v_{\text{tip}}$  is the growth rate of a dendrite tip at a certain undercooling,  $\alpha$  and  $\beta$  are the empirical constants.

## 2.3 Columnar to equiaxed transition (CET)

In general, after the molten metal is poured into the gap between the rolls, the nucleation will appear on the surface of rolls, and then many nuclei form. Since there is a forced heat stream on the surface of rolls, these nuclei will preferentially grow in the opposite direction of the forced heat stream. There will be internal nucleation when the liquid phase temperature of columnar crystals front achieves interior nucleation temperature  $T_i$ . According to the theory proposed by FLOOD and HUNT [14], in afterward solidification process, the dendrite growth will transform from columnar to equiaxed growth. The CET model is given as follows.

Center equiaxial crystal:

$$f_s(t) \geq f_1 \quad (3)$$

Equiaxed-columnar crystal:

$$f_2 < f_s(t) < f_1 \quad (4)$$

Columnar crystal:

$$f_s(t) \leq f_2 \quad (5)$$

$$f_s(t) = n(t) \cdot \frac{4}{3} \pi R_e^3(t) \cdot f_1(t) \quad (6)$$

where  $f_1=0.49$ ,  $f_2=0.0049$ ;  $n(t)$  is the grain density at each time-step;  $R_e(t)$  is the mean radius of equiaxed grain at each time-step;  $f_1(t)$  is the internal solid fraction at each time-step, which can be expressed as  $f_1(t)=\Omega(t)$ , where  $\Omega(t)$  is the solutal supersaturation of dendrite tip at each time-step.

All the control equations of twin-roll continuous casting, such as nucleation, equiaxed and columnar grain growth model, are shown as equations (1)–(6). Such as size of the equiaxed, columnar grain length and the process parameters affecting the solidification microstructure were achieved by certain calculations.

## 3 Computer emulational simulation of structures in solidification based on CA

According to the cellular automata model proposed by RAPPAZ and GANDIN [12], it may realize the kinetic simulator demonstration of the solidification structures in twin-roll continuous cast thin strip.

The freezing area is divided into quadrilateral or hexagonal grids, then each grid cell is divided into finer and uniform nodes, and all nodes before solidification is liquid ( $P_i=0$ ). When the cell temperature is lower than the liquidus, in a time step  $\delta t$ , the temperature decreases by  $\delta T$ , and the undercooling increases by  $\delta\Delta T(\delta\Delta T>0)$ . The new density of the nucleation in melt is given as:

$$\delta n_v = n_v(\Delta T + \delta T) - n_v(\Delta T) \quad (7)$$

These new grains are randomly distributed in the whole CA unit, and the probability is

$$p_v = \delta n_v \cdot V_{CA} \quad (8)$$

where  $n_v$  is the density of nuclei;  $\delta n_v$  is the density of nuclei each-time;  $V_{CA}$  is the volume of single CA unit;  $P_v$  is the volume nucleation on all CA units. Each CA unit is given one random number  $r$  ( $0 \leq r \leq 1$ ) in every time-step  $\delta t$ . If a unit is still liquid whose state index remains at 0, when  $r \leq P_v$ , the solid-liquid phase transition occurs, and its state index would be given a positive integer to describe the different grain orientations. When the CA unit nucleates, it will grow with a certain law. In numerical calculation, the approaches are as follows:  $A$  is a nucleation site in mesh grids which is nucleated at a certain time  $t_A$ , and  $\theta$  is the angle between the largest grain growth direction and  $x$ -axis. At time  $t$ , the radius of grain  $L(t)$  is the integral of growth velocity of dendrite tip in the whole growing time.

$$L(t) = \int_0^t v[\Delta T(t')] dt' \quad (9)$$

where the growth pattern of dendrite tip ( $v[\Delta T(t')]$ ) can be obtained by KGT model.

The sketch map of cellular automaton model is shown in Fig. 1. At the time  $t_B$ , the grain  $A$  grows and touches the four neighboring cells  $B_1$ ,  $B_2$ ,  $B_3$  and  $B_4$ . At this time, the semi-diagonal of grain  $L_{t_B}$  is equal to  $l_{\theta}=(\cos\theta+|\sin\theta|)$ , where  $l$  is the distance between two CA mesh grids. CA model prescribes that  $B_1$ ,  $B_2$ ,  $B_3$  and  $B_4$

are considered to become solid and assigned a crystallographic index as the same as *A*. The grain continues to grow and capture the neighboring liquid sites and form the final grain shape. *B*<sub>1</sub>, *B*<sub>2</sub>, *B*<sub>3</sub> and *B*<sub>4</sub> continue to grow and capture the eight sites of neighboring *C* at the next time. The grain increases with the growth velocity of dendrite tip.

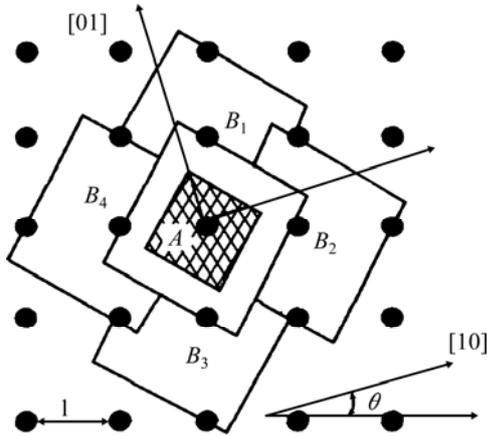


Fig. 1 Sketch map of cellular automaton model

**4 Validation of mathematical model**

The aluminum thin strip was chosen to validate the mathematical model. We may simplify the twin-roll continuous casting process of thin strip as the two-dimensional problem. The primary technical parameters of twin-roll casting are listed in Table 1. The thermo physical properties of aluminum needed for the model are listed in Table 2.

To reduce the calculation time, the computing region of solidification process should be simplified as a micro-unit (cube), whose dimensions are 0.5 mm×0.5 mm×1 mm. The model of simulation on solidification

**Table 1** Production condition and main parameters of twin-roll strip casting

Roll size/ mm	Roll gap/ mm	Casting speed/ (m·min <sup>-1</sup> )	Melt pool height/mm
d850×1500	5.9–6.1	0.8–1.2	40–100

**Table 2** Thermo-physical properties of aluminum [15]

<i>C</i> <sub>p,l</sub> / (J·kg <sup>-1</sup> ·°C <sup>-1</sup> )	<i>C</i> <sub>p,s</sub> / (J·kg <sup>-1</sup> ·°C <sup>-1</sup> )	<i>ρ</i> <sub>l</sub> / (kg·m <sup>-3</sup> )	<i>ρ</i> <sub>s</sub> / (kg·m <sup>-3</sup> )
1046	1138	2368	2700
<i>Γ</i> <sub>l</sub> / (W·m·°C <sup>-1</sup> )	<i>Γ</i> <sub>s</sub> / (W·m·°C <sup>-1</sup> )	<i>t</i> <sub>m</sub> / °C	<i>L</i> / (kJ·kg <sup>-1</sup> )
90.7	218	658.7	393.56

process of twin-roll continuous casting strip is shown in Fig. 2. The twin-roll continuous cast aluminum thin strip with the thickness of 6.0 mm was produced in the experiment. The simulated and experimental results of solidification microstructure of twin-roll continuous cast aluminum thin strip at the casting speed of 0.8 m/min and under the conditions of pouring temperature of 690 °C, melt pool height of 70 mm are shown in Figs. 3 and 4.

By analysis, the average grain size and the average columnar crystal deviation were measured, and the results are shown in Fig. 5. As a comparison, the predicted results of mathematical model are also shown in Fig. 5.

It is found from Figs. 4 and 5 that the predicted results are relatively consistent with the measured ones, indicating that the mathematic model is reliable thus can be used to predict the effects of processing parameters on the solidification structure of twin-roll continuous cast thin strips.

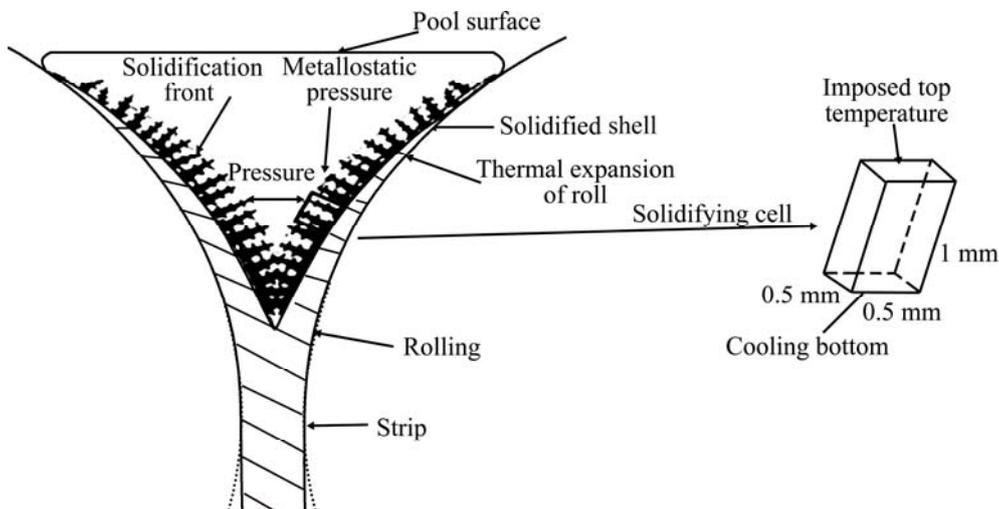
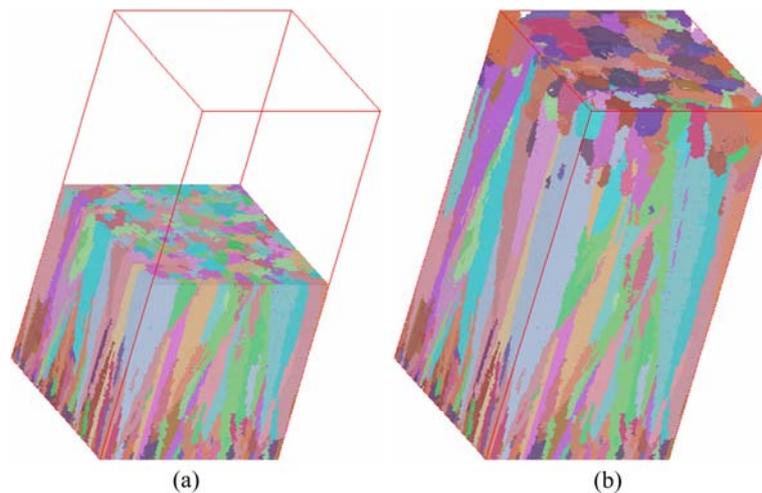
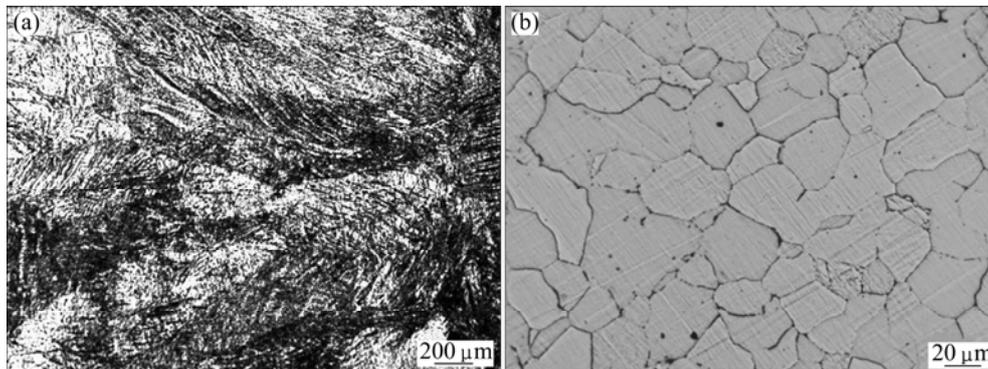


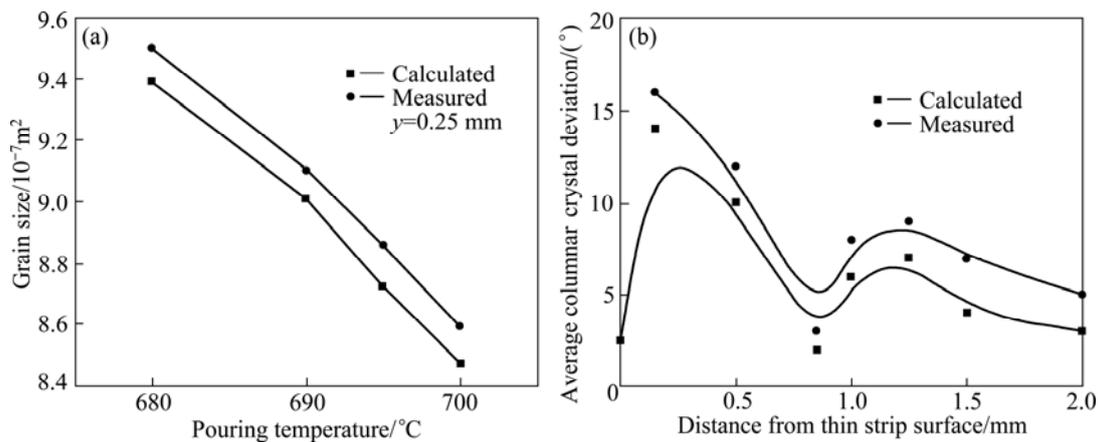
Fig. 2 Schematic of model of simulation on solidification process of twin-roll continuous cast thin strip



**Fig. 3** Simulated results of solidification microstructure of twin-roll continuous cast aluminum thin strip at casting speed of 0.8 m/min under conditions of pouring temperature of 690 °C, melt pool height of 70 mm: (a)  $t=5$  s; (b)  $t=10$  s



**Fig. 4** Microstructures of twin-roll continuous cast aluminum thin strip: (a) Solidified organization on cross section of aluminum strip; (b) Local magnification of (a)



**Fig. 5** Average grain size (a) and average columnar crystal deviation (b) of twin-roll continuous cast aluminum strip

## 5 Conclusions

1) A simple micro mathematical model for solidification structure simulation of twin-roll cast thin strip is developed. In the model, the latent heat is treated with the enthalpy method. Moreover, the heterogeneous

nucleation model, cellular automaton model and columnar-to-equiaxed transition models are also introduced, together with the revising of dendrite growth dynamic model of KGT. Although the predicted results of the micro mathematical model are relatively consistent with the measured ones, some errors still exist due to many assumptions in the model.

2) The average grain size and the average columnar crystal deviation were measured. The predicted results of the micro mathematical model are relatively consistent with the measured ones. It is shown that the established micro mathematical model is reliable, and it can predict influence of parameters on solidification structure of twin-roll continuous cast thin strip. The numerical simulation can provide some theoretical guidance for twin-roll continuous cast thin strip.

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# 铝双辊连续铸轧凝固微观组织的数值模拟

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**摘要:** 在研究双辊连铸纯铝薄带凝固过程的基础上, 基于金属凝固的基本原理, 并运用现代计算机仿真技术建立双辊连续铸轧纯铝薄带凝固的异质形核, 枝晶尖端的生长动力学(KGT), 柱状晶向等轴晶生长的转变(CET)的解析模型; 建立基于元胞自动机(CA)的双辊连铸纯铝薄带凝固组织的仿真模型, 为双辊连铸薄带凝固组织的仿真模拟奠定基础, 从而为双辊薄带连铸工艺提供一定的理论指导。同时, 利用双辊薄带连续铸轧纯铝凝固微观组织过程验证数学模拟的可行性。

**关键词:** 双辊连续铸轧; 凝固组织; 仿真模拟; 微观模型

(Edited by LI Xiang-qun)